### **EE6604**

# Personal & Mobile Communications

Week 7

Path Loss Models

Shadowing

Reading: 2.6, 2.7

### Okumura-Hata Model

$$L_p = \begin{cases} A + B \log_{10}(d) & \text{for urban area} \\ A + B \log_{10}(d) - C & \text{for suburban area} \\ A + B \log_{10}(d) - D & \text{for open area} \end{cases}$$

where

$$A = 69.55 + 26.16 \log_{10}(f_c) - 13.82 \log_{10}(h_b) - a(h_m)$$
  

$$B = 44.9 - 6.55 \log_{10}(h_b)$$
  

$$C = 5.4 + 2 [\log_{10}(f_c/28)]^2$$
  

$$D = 40.94 + 4.78 [\log_{10}(f_c)]^2 - 19.33 \log_{10}(f_c)$$

- Okumura and Hata's model is in terms of
  - carrier frequency  $150 \le f_c \le 1000 \text{ (MHz)}$
  - BS antenna height  $30 \le h_b \le 200 \text{ (m)}$
  - MS antenna height  $1 \le h_m \le 10 \text{ (m)}$
  - distance  $1 \le d \le 20$  (km) between the BS and MS.
- The model is known to be accurate to within 1 dB for distances ranging from 1 to 20 km.

• The parameter  $a(h_m)$  is a "correction factor"

$$a(h_m) = \begin{cases} (1.1 \log_{10}(f_c) - 0.7) h_m - (1.56 \log_{10}(f_c) - 0.8) \\ \text{for medium or small city} \\ \left\{ 8.28 \left( \log_{10}(1.54h_m) \right)^2 - 1.1 & \text{for } f_c \le 200 \text{ MHz} \\ 3.2 \left( \log_{10}(11.75h_m) \right)^2 - 4.97 & \text{for } f_c \ge 400 \text{ MHz} \\ \text{for large city} \end{cases} \end{cases}$$



Path loss predicted by the Okumura-Hata model. Large city,  $f_c = 900$  MHz,  $h_b = 70$  m,  $h_m = 1.5$  m.

# **CCIR** Model

• To account for varying degrees of urbanization, the CCIR (Comité International des Radio-Communication, now ITU-R) developed an empirical model for the path loss as:

$$L_{p (dB)} = A + B \log_{10}(d) - E$$

where A and B are defined in the Okumura-Hata model with  $a(h_m)$  being the medium or small city value.

• The parameter E accounts for the degree of urbanization and is given by

 $E = 30 - 25\log_{10}(\% \text{ of area covered by buildings})$ 

where E = 0 when the area is covered by approximately 16% buildings.

- Lee's area-to-area model is used to predict a path loss over flat terrain. If the actual terrain is not flat, e.g., hilly, there will be large prediction errors.
- Two parameters are required for Lee's area-to-area model; the power at a 1 mile (1.6 km) point of interception,  $\mu_{\Omega_p}(d_o)$ , and the path-loss exponent,  $\beta$ .
- $\bullet$  The received signal power at distance d can be expressed as

$$\mu_{\Omega_p}(d) = \mu_{\Omega_p}(d_o) \left(\frac{d}{d_o}\right)^{-\beta} \left(\frac{f}{f_o}\right)^{-n} \alpha_0$$

or in decibel units

$$\mu_{\Omega_p \ (\text{dBm})}(d) = \mu_{\Omega_p \ (\text{dBm})}(d_o) - 10\beta \log_{10}\left(\frac{d}{d_o}\right) - 10n \log_{10}\left(\frac{f}{f_o}\right) + 10 \log_{10}\alpha_0 \ ,$$

where d is in units of kilometers and  $d_o = 1.6$  km.

• The parameter  $\alpha_0$  is a correction factor used to account for different BS and MS antenna heights, transmit powers, and antenna gains.

- The following set of *nominal* conditions are assumed in Lee's area-to-area model:
  - frequency  $f_o = 900 \text{ MHz}$
  - BS antenna height = 30.48 m
  - BS transmit power = 10 watts
  - BS antenna gain  $= 6~\mathrm{dB}$  above dipole gain
  - MS antenna height = 3 m
  - MS antenna gain= 0 dB above dipole gain
- If the actual conditions are different from those listed above, then we compute the following parameters:

$$\alpha_{1} = \left(\frac{\text{BS antenna height (m)}}{30.48 \text{ m}}\right)^{2}$$

$$\alpha_{2} = \left(\frac{\text{MS antenna height (m)}}{3 \text{ m}}\right)^{\kappa}$$

$$\alpha_{3} = \frac{\text{transmitter power}}{10 \text{ watts}}$$

$$\alpha_{4} = \frac{\text{BS antenna gain with respect to } \lambda_{c}/2 \text{ dipole}}{4}$$

$$\alpha_{5} = \text{different antenna-gain correction factor at the MS}$$

• The parameters  $\beta$  and  $\mu_{\Omega_p}(d_o)$  have been found from empirical measurements, and are listed in the Table below.

Terrain	$\mu_{\Omega_p}(d_o)~(\mathrm{dBm})$	$\beta$
Free Space	-45	2
Open Area	-49	4.35
North American Suburban	-61.7	3.84
North American Urban (Philadelphia)	-70	3.68
North American Urban (Newark)	-64	4.31
Japanese Urban (Tokyo)	-84	3.05

- For  $f_c < 450$  MHz in a suburban or open area, n = 2 is recommended. In an urban area with  $f_c > 450$  MHz, n = 3 is recommended.
- The value of  $\kappa$  in is also determined from empirical data as

$$\kappa = \begin{cases} 2 & \text{for a MS antenna height} > 10 \text{ m} \\ 3 & \text{for a MS antenna height} < 3 \text{ m} \end{cases}$$

- The path loss  $L_{p (dB)}$  is the difference between the transmitted and received field strengths,  $L_{p (dB)} = \mu_{\Omega_{p (dBm)}}(d) - \mu_{\Omega_{t (dBm)}}.$
- To compare with the Okumura-Hata model, we assume a half wave dipole BS antenna, so that  $\alpha_4 = -6$  dB.
- Then by using the same parameters as before,  $h_b = 70$  m,  $h_m = 1.5$ m,  $f_c = 900$  MHz, a nominal BS transmitter power of 40 dBm (10 watts), and the parameters in the Table for  $\mu_{\Omega_p (dBm)}(d_o)$  and  $\beta$ , the following path losses are obtained:

$$L_{p (dB)} = \begin{cases} 85.74 + 20.0 \log_{10} d & \text{Free Space} \\ 84.94 + 43.5 \log_{10} d & \text{Open Area} \\ 98.68 + 38.4 \log_{10} d & \text{Suburban} \\ 107.31 + 36.8 \log_{10} d & \text{Philadelphia} \\ 100.02 + 43.1 \log_{10} d & \text{Newark} \\ 122.59 + 30.5 \log_{10} d & \text{Tokyo} \end{cases}$$



Path loss obtained by using Lee's method;  $h_b = 70 m$ ,  $h_m = 1.5 m$ ,  $f_c = 900 Mhz$ , and an isotropic BS antenna.

## COST231-Hata Model

- COST231 models are for propagation in the PCS band.
- Path losses experienced at 1845 MHz are about 10 dB larger than those experienced at 955 MHz.
- The COST-231 Hata model for NLOS propagation is

$$L_p = A + B\log_{10}(d) + C$$

where

$$A = 46.3 + 33.9 \log_{10}(f_c) - 13.82 \log_{10}(h_b) - a(h_m)$$
  

$$B = 44.9 - 6.55 \log_{10}(h_b)$$
  

$$C = \begin{cases} 0 & \text{medium city and suburban areas} \\ & \text{with moderate tree density} \\ 3 & \text{for metropolitan centers} \end{cases}$$

### COST231-Walfish-Ikegami LOS Model

• For LOS propagation in a street canyon, the path loss is

$$L_p = 42.6 + 26\log_{10}(d) + 20\log_{10}(f_c), \quad d \ge 20 \ m$$

where the first constant is chosen so that  $L_p$  is equal to the free-space path loss at a distance of 20 m.

• The model parameters are the distance d (km) and carrier frequency  $f_c$  (MHz).

## COST231-Walfish-Ikegami NLOS Model



Definition of parameters used in the COST231-Walfish-Ikegami model.

• For NLOS propagation, the path loss is composed of three terms, viz.,

$$L_p = \begin{cases} L_o + L_{\text{rts}} + L_{\text{msd}} & \text{for } L_{\text{rts}} + L_{\text{msd}} \ge 0\\ L_o & \text{for } L_{\text{rts}} + L_{\text{msd}} < 0 \end{cases}$$

– The free-space loss is

$$L_o = 32.4 + 20\log_{10}(d) + 20\log_{10}(f_c)$$

- The roof-top-to-street diffraction and scatter loss is

$$L_{\rm rts} = -16.9 - 10\log_{10}(w) + 10\log_{10}(f_c) + 20\log_{10}\Delta h_m + L_{\rm ori}$$

where

$$L_{\text{ori}} = \begin{cases} -10 + 0.354(\phi) , & 0 \le \phi \le 35^{\circ} \\ 2.5 + 0.075(\phi - 35) , & 35 \le \phi \le 55^{\circ} \\ 4.0 - 0.114(\phi - 55) , & 55 \le \phi \le 90^{\circ} \\ \Delta h_m = h_{\text{Roof}} - h_m \end{cases}$$

• The multi-screen diffraction loss is

$$L_{\rm msd} = L_{\rm bsh} + k_a + k_d \log_{10}(d) + k_f \log_{10}(f_c) - 9\log_{10}(b)$$

where

$$L_{\rm bsh} = \begin{cases} -18\log_{10}(1 + \Delta h_b) & h_b > h_{\rm Roof} \\ 0 & h_b \le h_{\rm Roof} \end{cases}$$

$$k_a = \begin{cases} 54 , & h_b > h_{\rm Roof} \\ 54 - 0.8\Delta h_b , & d \ge 0.5 \text{km and } h_b \le h_{\rm Roof} \\ 54 - 0.8\Delta h_b d/0.5 , & d < 0.5 \text{km and } h_b \le h_{\rm Roof} \end{cases}$$

$$k_d = \begin{cases} 18 , & h_b > h_{\rm Roof} \\ 18 - 15\Delta h_b/h_{\rm Roof} , & h_b \le h_{\rm Roof} \\ 18 - 15\Delta h_b/h_{\rm Roof} , & h_b \le h_{\rm Roof} \end{cases}$$

$$k_f = -4 + \begin{cases} 0.7(f_c/925 - 1) , & \text{medium city and suburban} \\ 1.5(f_c/925 - 1) , & \text{metropolitan area} \end{cases}$$

and

$$\Delta h_b = h_b - h_{\rm Roof} \ .$$

- $k_a$  is the increase in path loss for BS antennas below the roof tops of adjacent buildings.
- $k_d$  and  $k_f$  control the dependency of the multi-screen diffraction loss on the distance and frequency, respectively.
- The model is valid for the following ranges of parameters,  $800 \le f_c \le 2000 \text{ (MHz)}, 4 \le h_b \le 50 \text{ (m)}, 1 \le h_m \le 3 \text{ (m)}, \text{ and } 0.02 \le d \le 5 \text{ (km)}.$
- The following default values are recommended, b = 20...50 (m), w = b/2,  $\phi = 90^{\circ}$ , and  $h_{\text{Roof}} = 3 \times \text{number of floors} + \text{roof (m)}$ , where roof = 3 (m) pitched and 0 (m) flat.

# **3GPP 3-D Path Loss Models**

- The 3GPP path loss models are valid from 2 to 6 GHz for different BS and MS antenna heights.
- The 3GPP path loss models are categorized into urban macrocell (UMa) and urban microcell (UMi) cases, corresponding to BS antenna heights of 25 m or less and 25 m or more, respectively.
- The UMa and UMi cases are further categorized into LoS, NLoS, and outdoor-to-indoor scenarios.
- The distance definitions are defined below for outdoor scenarios and for outdoor-indoor scenarios.

### **3GPP 3-D** Path Loss Model Distance Definitions



Definition of  $d_{2D}$  and  $d_{3D}$  for outdoor mobile stations.



Definition of  $d_{2Dout}$ ,  $d_{2Din}$ ,  $d_{3Dout}$  and  $d_{3Din}$  for indoor mobile stations.

### LoS Probability

• The various 3GPP path loss models make use of the probability of LoS condition. For microcells and outdoor MSs, the probability of LoS is

$$P_{LoS} = min(18/d_{2D}, 1)(1 - e^{-d_{2D}/36}) + e^{-d_{2D}/36}$$

- For microcells and indoor MSs, the above formula is used with  $d_{2D}$  replaced by  $d_{2Dout}$ .
- For macrocells and outdoor MSs, the probability of LoS is

$$P_{\text{LoS}} = \left(\min(18/d_{2D}, 1)(1 - e^{-d_{2D}/63}) + e^{-d_{2D}/63}\right) \left(1 + C(d_{2D}, h_m)\right)$$

where

$$C(d_{2D}, h_m) = \begin{cases} 0 & , h_m < 13 \ m \\ \left(\frac{h_m - 13}{10}\right)^{1.5} g(d_{2D}) & , 13 \ m \le h_m \le 23 \ m \end{cases}$$

and

$$g(d_{2D}) = \begin{cases} (1.25e^{-6})d_{2D}^2e^{d_{2D}/150} &, d_{2D} > 18 m \\ 0 &, \text{ otherwise} \end{cases}$$

• For macrocells and indoor MSs, the above formulas are used with  $d_{2D}$  replaced by  $d_{2Dout}$ .

### 3GPP 3D-UMa LoS

• For macrocells with LoS conditions

 $L_{\rm UMaLoS~(dB)} ~=~ 22.0 \log_{10}(d_{3D}) + 28.0 + 20 \log_{10}(f_c) ~,~~ 10~m < d_{2D} < d_{BP}$ 

$$L_{\text{UMaLoS (dB)}} = 40 \log_{10}(d_{3D}) + 28.0 + 20 \log_{10}(f_c) - 9 \log_{10}\left(d_{BP}^2 + (h_b - h_m)^2\right) ,$$
  
$$d_{BP} < d_{2D} < 5000 \ m; \ h_b = 25 \ m; \ 1.5 \ m \le h_m \le 22.5 \ m$$

- The break point distance is given by  $d_{BP} = 4h_b h_m f_c/c$  corresponding to the last local maxima in the flat earth model. In the 3D-UMa scenario the effective antenna heights  $h_b$  and  $h_m$ are computed as follows:  $h_b = \hat{h}_b - h_E$ ,  $h_m = \hat{h}_m - h_E$ , where  $\hat{h}_b$  and  $\hat{h}_m$  are the actual antenna heights, and the effective environment height  $h_E$  depends on the link between a BS and a MS. For LoS links,  $h_E = 1 m$  with probability  $1/(1 + C(d_{2D}, h_m))$ , where the function  $C(d_{2D}, h_m)$  is defined earlier. Otherwise,  $h_E$  is chosen from a discrete uniform distribution on the set  $\{12, 15, \ldots, (h_m - 1.5)\}$ .
- The shadow standard deviation is  $\sigma_{\Omega} = 4$  dB.

# 3GPP 3D-UMa NLoS

• For macrocells with NLoS conditions

$$L_{\text{UMaNLoS (dB)}} = \max \left\{ L_{\text{UMaNLoS (dB)}}, L_{\text{UMaLoS (dB)}} \right\}$$
,

where

$$L_{\text{UMaNLoS (dB)}} = 161.04 - 7.1 \log_{10}(W) + 7.5 \log_{10}(h_{\text{build}}) - (24.37 - 3.7(h_{\text{build}}/h_b)^2) \log_{10}(h_b) + (43.42 - 3.1 \log_{10}(h_b)) (\log_{10}(d_{3D}) - 3) + 20 \log_{10}(f_c) - (3.2(\log_{10}(17.625))^2 - 4.97) - 0.6(h_m - 1.5)$$

and

10 
$$m < d_{2D} < 5,000 m$$
  
 $h_{\text{build}} = \text{average building height}$   
 $W = \text{street width}$   
 $h_b = 25 m, 1.5 m \le h_m \le 22.5 m, W = 20 m, h_{\text{build}} = 20 m$   
Applicable ranges:  
 $5 m < h_{\text{build}} < 50 m$   
 $5 m < W < 50 m$   
 $10 m < h_b < 150 m$   
 $1.5 m \le h_m \le 22.5 m$ 

• The shadow standard deviation is  $\sigma_{\Omega} = 6$  dB.

## 3GPP 3D-UMa O-to-I

• For macrocells with outdoor-to-indoor conditions

$$L_{\text{UMaO-to-I (dB)}} = L_{\text{b (dB)}} + L_{\text{tw (dB)}} + L_{\text{in (dB)}}$$

For a hexagonal cell layout:

$$L_{\rm b (dB)} = L_{\rm UMa (dB)} (d_{3D-out} + d_{3D-in})$$
  

$$L_{\rm tw (dB)} = 20 \text{ (loss through wall)}$$
  

$$L_{\rm in (dB)} = 0.5d_{2D-in} \text{ (inside loss)}$$

where

$$\begin{array}{l} 10 \ m < d_{2D-out} + d_{2D-in} < 1000 \ m \\ 0 \ m < d_{2D-in} < 25 \ m \\ h_b = 25 \ m, h_m = 3(n_{fl} - 1) + 1.5 \ , \ n_{fl} = 1, 2, 3, 4, 5, 6, 7, 8 \\ d_{2D-in} \ \text{is assumed uniformly distributed between 0 and } 25 \ . \end{array}$$

- The shadow standard deviation is  $\sigma_{\Omega} = 7$  dB.
- The building penetration loss (BPL) or "loss through wall" in the 3GPP 3D-UMa O-to-I model is 20 dB. However, this will vary greatly depending on the building. Moreover, the building penetration loss increases with frequency. An empirical BPL model is

$$BPL_{(dB)} = 10 \log_{10} \left( A + B f_c^2 \right)$$

where  $f_c$  is the frequency in GHz, A = 5 and B = 0.03 for low loss buildings and A = 10 and B = 5 for high loss buildings.

# 3GPP 3D-UMi LoS, NLoS and 3D-UMi O-to-I

- The microcell LoS path loss is the same as the macrocell LoS path loss  $L_{\text{UMaLOS (dB)}}$ , except that  $h_E = 1 \ m$  with probability one and the shadow standard deviation is  $\sigma_{\Omega} = 3 \text{ dB}$ .
- For NLoS and a hexagonal cell layout

$$L_{\text{UMiNLoS (dB)}} = \max \left\{ L_{\text{UMiNLoS (dB)}}, L_{\text{UMiLoS (dB)}} \right\} ,$$

where

$$L_{\text{UMiNLoS (dB)}} = 36.7 \log_{10}(d_{3D}) + 22.7 + 26 \log_{10}(fc) - 0.3(h_m - 1.5)$$

10 
$$m < d_{2D} < 2000 m$$
  
 $h_b = 10 m$   
 $1.5 m \le h_m \le 22.5m$ 

The shadow standard deviation is  $\sigma_{\Omega} = 4$  dB.

• The microcell outdoor-to-indoor path loss is the same as the macrocell outdoor-to-indoor path loss  $L_{\text{UMaO-to-I}(\text{dB})}$ , except that  $h_b = 10$  m instead of  $h_b = 25$  m. The shadow standard deviation remains at  $\sigma_{\Omega} = 7$  dB.

## Shadowing

• Shadows are very often modeled as being log-normally distributed.

• Let

$$\Omega_v = \mathbf{E}[\alpha(t)], \qquad \mu_{\Omega_v} = \mathbf{E}[\Omega_v]$$
  
$$\Omega_p = \mathbf{E}[\alpha^2(t)], \qquad \mu_{\Omega_p} = \mathbf{E}[\Omega_p]$$

• Then distributions of  $\Omega_v$  and  $\Omega_p$  are

$$p_{\Omega_{v}}(x) = \frac{2\xi}{x\sigma_{\Omega}\sqrt{2\pi}} \exp\left\{-\frac{\left(10\log_{10}x^{2} - \mu_{\Omega_{v}}\right)^{2}}{2\sigma_{\Omega}^{2}}\right\}$$
$$p_{\Omega_{p}}(x) = \frac{\xi}{x\sigma_{\Omega}\sqrt{2\pi}} \exp\left\{-\frac{\left(10\log_{10}x - \mu_{\Omega_{p}}\right)^{2}}{2\sigma_{\Omega}^{2}}\right\}$$

where

$$\mu_{\Omega_{v (dBm)}} = 10 \mathbb{E}[\log_{10} \Omega_{v}^{2}]$$
$$\mu_{\Omega_{p (dBm)}} = 10 \mathbb{E}[\log_{10} \Omega_{p}]$$

and  $\xi = \ln 10/10$ .

### Shadowing

• By using a transformation of random variables,  $\Omega_{v (dBm)} = 10 \log_{10} \Omega_v^2$  and  $\Omega_{p (dBm)} = 10 \log_{10} \Omega_p$  have the Gaussian densities

$$p_{\Omega_{v (dBm)}}(x) = \frac{1}{\sqrt{2\pi}\sigma_{\Omega}} \exp\left\{-\frac{(x-\mu_{\Omega_{v (dBm)}})^{2}}{2\sigma_{\Omega}^{2}}\right\}$$
$$p_{\Omega_{p (dBm)}}(x) = \frac{1}{\sqrt{2\pi}\sigma_{\Omega}} \exp\left\{-\frac{(x-\mu_{\Omega_{p (dBm)}})^{2}}{2\sigma_{\Omega}^{2}}\right\}$$

• Note that the standard deviation  $\sigma_{\Omega}$  of  $\Omega_{v (dBm)}$  and  $\Omega_{p (dBm)}$  are the same. However, for Rician fading channels the means differ by

$$\mu_{\Omega_p (\mathrm{dBm})} = \mu_{\Omega_v (\mathrm{dBm})} + 10 \cdot \log_{10} C(K)$$

where

$$C(K) = \frac{4e^{2K}(K+1)}{\pi_1 F_1^2(3/2,1;K)}$$

 $_1F_1(\cdot, \cdot; \cdot)$  is the confluent hypergeometric function (see Chap. 2, Appendix 3).

• Note that  $C(0) = 4/\pi$ ,  $C(\infty) = 1$ , and  $1 \le C(K) \le 4/\pi$  for  $0 \le K \le \infty$ .

# **Shadow Simulation**

- Shadows can be modelled by low-pass filtering white noise.
  - Here we suggest a first-order low pass digital filter.
- In a discrete-time simulation, the local mean  $\Omega_{k+1 (dBm)}$  at step k+1 is generated recursively as follows:

$$\Omega_{k+1 (\mathrm{dBm})} = \xi \Omega_{k (\mathrm{dBm})} + (1-\xi)v_k$$

- -k is the step index.
- $-\{v_k\}$  is a sequence of independent zero-mean Gaussian random variables with variance  $\tilde{\sigma}^2$ .
- $\xi$  controls the shadow correlation
- The autocorrelation function of  $\Omega_{k \text{ (dBm)}}$  can be derived as:

$$\phi_{\Omega_{\rm (dBm)}\Omega_{\rm (dBm)}}(n) = \frac{1-\xi}{1+\xi} \tilde{\sigma}^2 \xi^{|n|}$$

• The variance of log-normal shadowing is

$$\sigma_{\Omega}^{2} = \phi_{\Omega_{(\mathrm{dBm})}\Omega_{(\mathrm{dBm})}}(0) = \frac{1-\xi}{1+\xi}\tilde{\sigma}^{2}$$

– Consequently, we can express the autocorrelation of  $\Omega_k$  as

$$\phi_{\Omega_{(\mathrm{dBm})}\Omega_{(\mathrm{dBm})}}(n) = \sigma_{\Omega}^2 \xi^{|n|}$$

- Notice that the shadows decorrelated exponentially with the time lag in the autocorrelation function.
- $\bullet$  Suppose we use discrete-time simulation, where each simulation step corresponds to T seconds.
  - For a mobile station traveling at velocity v, the distance traveled in T seconds is vT meters.
  - Let  $\xi_D$  be the shadow correlation between two points separated by a spatial distance of D meters.
  - Then the time autocorrelation of the shadowing is

$$\phi_{\Omega_{\rm (dBm)}\Omega_{\rm (dBm)}}(n) \equiv \phi_{\Omega_{\rm (dBm)}\Omega_{\rm (dBm)}}(nT) = \sigma_{\Omega}^2 \xi_D^{(vT/D)|n|}$$

- Measurements in Stockholm have shown  $\xi_D = 0.1$  for D = 30 meters (roughly). However, this can vary greatly depending on local topography.