

# EE4061

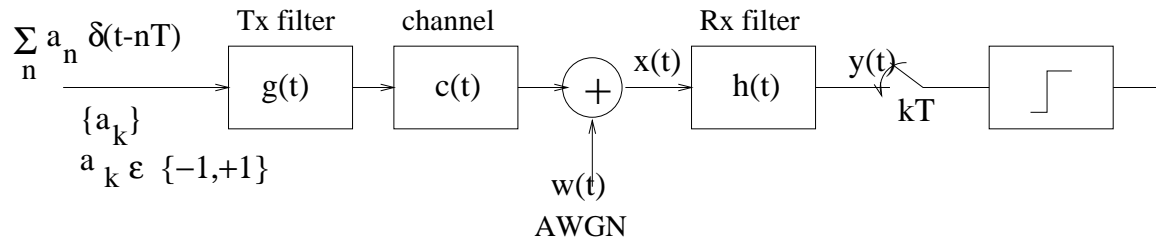
# Communication Systems

Week 10

Intersymbol Interference

Nyquist Pulse Shaping

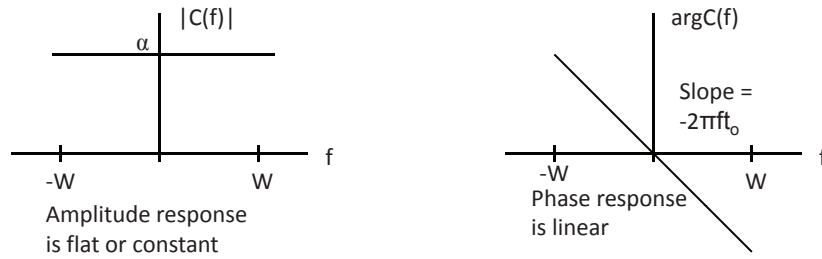
# Intersymbol Interference (ISI)



An ideal channel  $c(t)$  only scales and time shifts the signal  $g(t)$ , but otherwise leaves it undistorted, i.e. for an ideal channel

$$\begin{aligned}c(t) &= \alpha \delta(t - t_o) \\g(t) * c(t) &= \alpha g(t - t_o) \\C(f) &= \alpha e^{-j2\pi f t_o}\end{aligned}$$

# ISI



Let

$$\begin{aligned} p(t) &= g(t) * c(t) * h(t) \\ &\updownarrow \\ P(f) &= G(f)C(f)H(f) \end{aligned}$$

Then  $y(t) = \sum_n a_n p(t - nT) + n(t)$ , where  $n(t) = w(t) * h(t)$

# ISI

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$$\begin{aligned}y_i = y(iT) &= \sum_n a_n p((i-n)T) + n(iT) \\ &= \sum_n a_n p_{i-n} + n_i\end{aligned}$$

where  $p_{i-n} = p((i-n)T)$ ,  $n_i = nT$

$$y_i = a_i p_0 + \sum_{n \neq i} a_n p_{i-n} + n_i$$

$a_i p_0$  – desired term,

$\sum_{n \neq i} a_n p_{i-n}$  – ISI

$n_i$  – noise

In the absence of ISI and noise,  $y_i = a_i p_0$ . Any pulse  $p(t)$  with

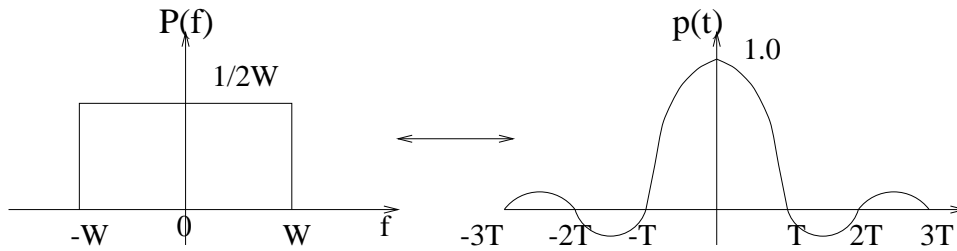
$$p_i = p(iT) = \begin{cases} p_0 & i = 0 \\ 0 & i \neq 0 \end{cases} = p_0 \delta_{i0}$$

yields zero ISI

# Bandlimited Pulse Shaping

What pulse shapes  $p(t)$ ,  $p(t) = g(t) * c(t) * h(t)$  yield zero ISI.

Suppose  $P(f) = \frac{1}{2W} \text{rect}\left(\frac{f}{2W}\right)$  where  $W = 1/2T = R/2$ ,  $T$  is the baud duration,  $R$  is the baud rate



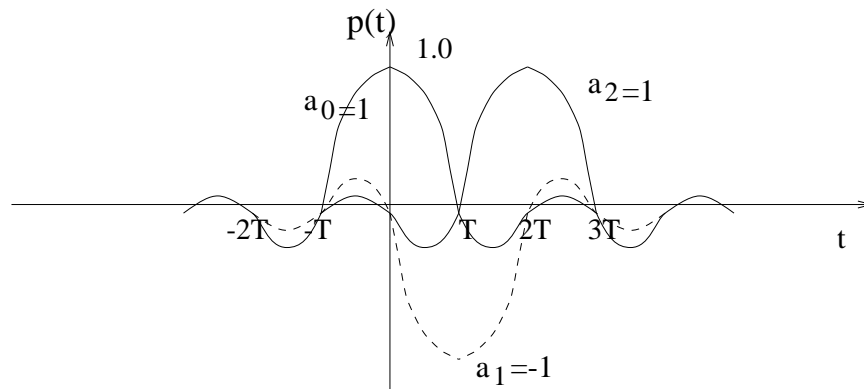
$$p(t) = \text{sinc}(2Wt) = \text{sinc}(t/T), \quad T = 1/2W$$

Note that

$$\begin{aligned} p_i = p(iT) &= \begin{cases} 1 & i = 0 \\ 0 & i \neq 0 \end{cases} \\ &= \delta_{i0} \end{aligned}$$

This pulse results in zero ISI. Note that  $p(t)$  is noncausal

# ISI - Problems



## Problems:

1.  $P(f) = \frac{1}{2W} \text{rect} \left( \frac{f}{2W} \right)$  is not realizable
2.  $p(t)$  decays slowly with time. It decreases with  $1/|t|$  for large  $t$ . Therefore, it is very sensitive to sampler phase

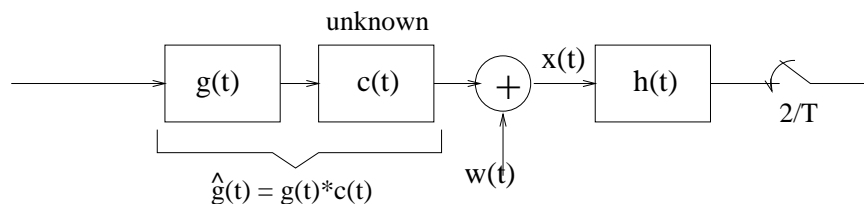
# Problems with 'sinc' pulse

$$\begin{aligned}y(t) &= \sum_n a_n p(t - nT) \\y(\Delta t) &= \sum_n a_n p(\Delta t - nT) \\&= \sum_n a_n \frac{\sin[\pi(\Delta t - nT)/T]}{\pi(\Delta t - nT)/T} \\&= \sum_n \frac{\sin(\pi\Delta t/T) \cos(\pi n) - \cos(\pi\Delta t/T) \sin(\pi n)}{\pi\Delta t/T - n\pi} \\&= \sum_n a_n \frac{(-1)^n \sin(\pi\Delta t/T)}{\pi\Delta t/T - n\pi} \\&= a_0 \operatorname{sinc}(\Delta t/T) + \frac{\sin(\pi\Delta t/T)}{\pi} \sum_{n \neq 0} \frac{a_n (-1)^n}{\Delta t/T - n}\end{aligned}$$

Last term is not absolutely summable.

We have seen  $y_i = y(iT) = a_i p_0 + \sum_{n \neq i} a_n p_{i-n} + n_i$   
where  $p_k = p(kT)$ ,  $n_i = n(iT)$ .

# Matched Filtering and Pulse Shaping



- To maximize the signal-to-noise ratio at the output of the receiver filter  $h(t)$ , in theory we match the receiver filter to the received pulse  $\hat{g}(t) = g(t) * c(t)$ , i.e.,  $h(t) = \tilde{g}(T - t)$ . However, if  $c(t)$  is unknown, then so is  $h(t)$ .
- Practical Solution: Choose  $h(t)$  matched to the transmitted pulse  $g(t)$ , i.e., choose  $h(t) = g(T - t)$ , over-sample by a factor of 2, and process 2 samples per baud interval.
  - This is optimal, similar to the case when  $c(t)$  is known, but the proof is beyond the scope of this course.



# Matched Filtering and Pulse Shaping

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- To design the transmit and receiver filters, we will assume an ideal channel  $c(t) = \delta(t)$ , so that the overall pulse (ignoring time delay) is

$$\begin{aligned} p(t) &= g(t) * h(t) \\ &= g(t) * g(-t) \end{aligned}$$

- Taking the Fourier transform of both sides

$$P(f) = G(f)G^*(f) = |G(f)|^2$$

- Hence

$$|G(f)| = \sqrt{|P(f)|}$$

- For many practical pulses,  $g(t)$ , we will also see that  $g(t) = g(-t)$ , i.e., the pulse is even in  $t$ , so that  $h(t) = g(t)$ .

# Conditions for ISI free transmission

The condition for ISI-free transmission is

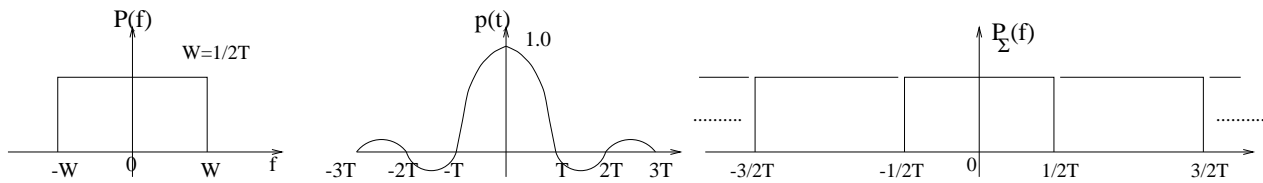
$$p_k = \delta_{k0}p_0 = \begin{cases} p_0 & k = 0 \\ 0 & k \neq 0 \end{cases}$$

That is,  $p(t)$  must have equally spaced zero crossings, separated by  $T$  seconds.

Theorem: The pulse  $p(t)$  satisfies  $p_k = \delta_{k0}p_0$  iff

$$P_{\Sigma}(f) \triangleq \frac{1}{T} \sum_{n=-\infty}^{\infty} P(f + n/T) = p_0$$

That is the folded spectrum  $P_{\Sigma}(f)$  is flat.



# ISI free transmission

Proof:

$$\begin{aligned} p_k &= \int_{-\infty}^{\infty} P(f) e^{j2\pi f k T} df \\ &= \sum_{n=-\infty}^{\infty} \int_{(2n-1)/2T}^{(2n+1)/2T} P(f) e^{j2\pi f k T} df \quad f' = f - n/T \\ &= \sum_{n=-\infty}^{\infty} \int_{-1/2T}^{1/2T} P(f' + n/T) e^{j2\pi k(f'+n/T)T} df' \\ &= \int_{-1/2T}^{1/2T} e^{j2\pi f' k T} \left[ \sum_{n=-\infty}^{\infty} P(f' + n/T) \right] df' \end{aligned} \quad (1)$$

To prove sufficiency, we assume that  $\sum_{n=-\infty}^{\infty} P(f' + n/T) = p_0 T$  is true. Then,

$$p_k = p_0 T \int_{-1/2T}^{1/2T} e^{j2\pi f' k T} df' = \frac{\sin \pi k}{\pi k} p_0 = \delta_{k0} p_{k0}$$

To prove necessity, we have from (1)

$$p_k = T \int_{-1/2T}^{1/2T} P_{\Sigma}(f') e^{j2\pi f' k T} df'$$

# Nyquist Pulse

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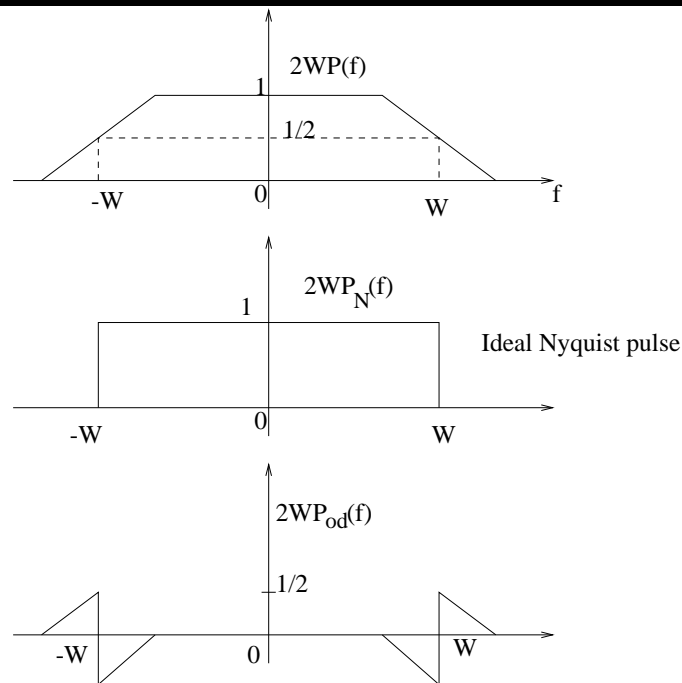
Hence,  $p_k$  and  $P_\Sigma(f)$  are a Fourier series pair, i.e.,

$$P_\Sigma(f) = \sum_{k=-\infty}^{\infty} p_k e^{j2\pi f k T}$$

If  $p_k = p_0 \delta_{k0}$  is assumed true, then from the above equation  $P_\Sigma(f) = p_0$ .

- Nyquist Pulse Shaping: A pulse  $p(t)$  that yields zero-ISI is one having a folded spectrum that is flat.
  - The pulse  $p(t)$  can be generated by choosing  $P(f)$  as shown on the following slide.

# Nyquist Pulse Shaping

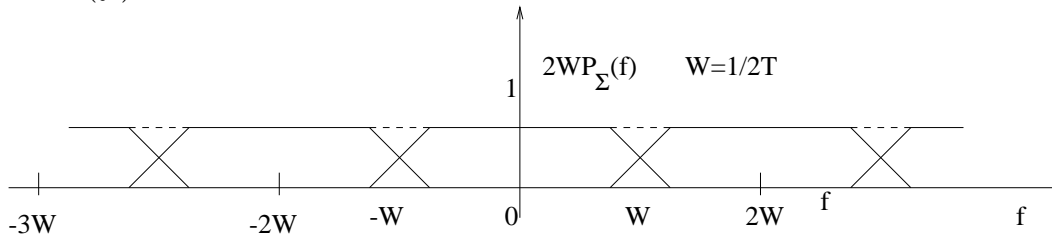


Note  $P(f) = P_N(f) + P_{od}(f)$ .

$P_{od}(f)$  can be any function that has skew symmetry about  $f = W$ .

# Nyquist Pulse

Note that  $P_{\Sigma}(f)$  is flat under this condition.



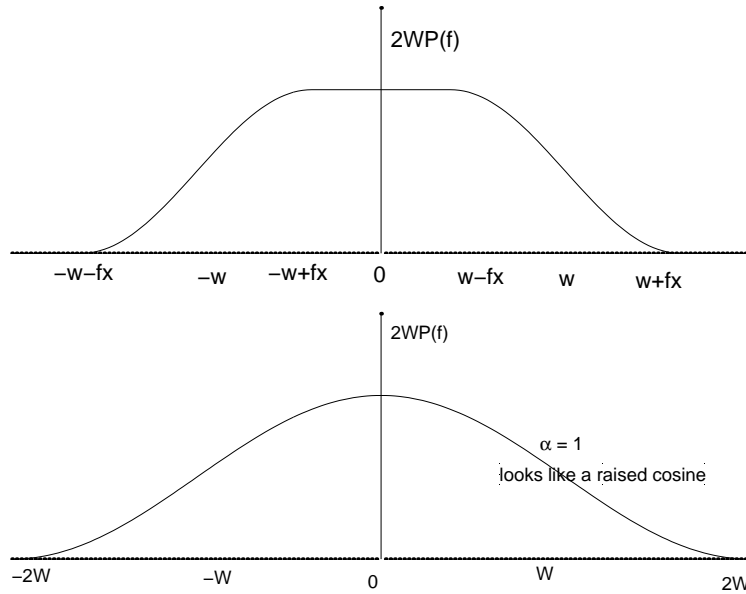
Example: Raised Cosine

$$2WP_{od}(f) = \begin{cases} -\frac{1}{2} - \frac{1}{2} \sin \frac{\pi(|f|-W)}{2f_x} & W - f_x \leq |f| \leq W \\ \frac{1}{2} - \frac{1}{2} \sin \frac{\pi(|f|-W)}{2f_x} & W \leq |f| \leq W + f_x \end{cases}$$

$f_x$  = bandwidth expansion,  $\frac{f_x}{W} \times 100 =$  excess bandwidth (%),  $\alpha = \frac{f_x}{W} =$  roll off factor

$$2WP(f) = \begin{cases} 1 & 0 \leq |f| \leq W - f_x \\ \frac{1}{2} \left[ 1 - \sin \frac{\pi(|f|-W)}{2f_x} \right] & W - f_x \leq |f| \leq W + f_x \\ 0 & |f| \geq W + f_x \end{cases}$$

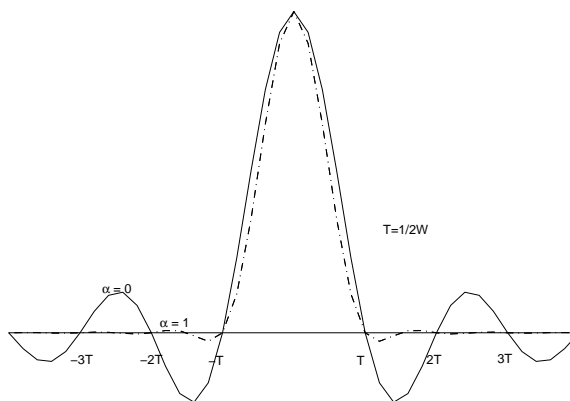
# Raised Cosine Pulse



# Raised Cosine Impulse Response

Impulse response - Since  $P(f)$  is even, the inverse cosine transform yields

$$\begin{aligned} p(t) &= 2 \int_0^{W+f_x} P(f) \cos 2\pi f t d f \\ &= 2 \cdot \frac{1}{2W} \int_0^{W-f_x} \cos 2\pi f t d f + 2 \cdot \frac{1}{2W} \int_{W-f_x}^{W+f_x} \frac{1}{2} \left[ 1 - \sin \frac{\pi|f| - W}{2f_x} \right] \cos 2\pi f t d f \\ &= \frac{\sin 2\pi W t}{2\pi W t} \cdot \frac{\cos 2\pi f_x t}{1 - (4f_x t)^2} \end{aligned}$$





# Square Root Raised Cosine Pulse

- To implement a matched filter, we split the overall pulse  $P(f)$  between the transmit and receive filters, i.e.,  $p(t) = g(t) * g(-t)$ .
- We have seen earlier that  $P(f) = G(f)G^*(f) = |G(f)|^2$ , so that  $|G(f)| = \sqrt{P(f)}$ .
- With square-root raised cosine pulse shaping

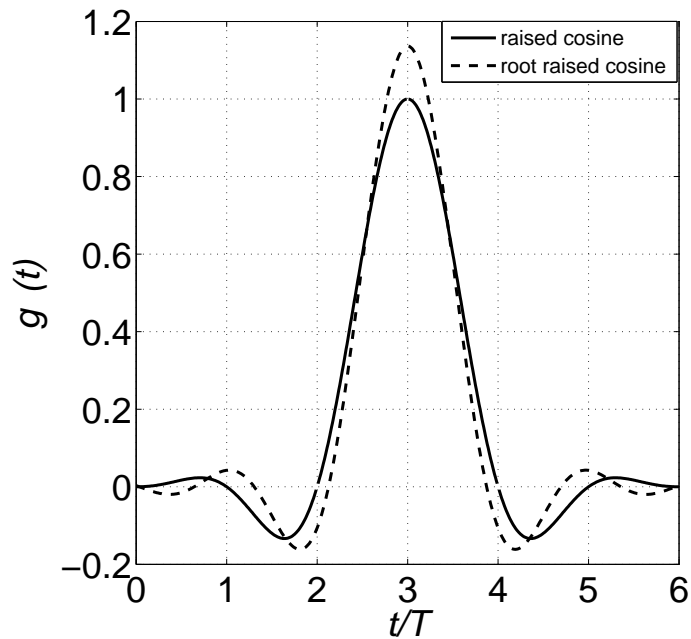
$$\sqrt{2W}|G(f)| = \begin{cases} 1 & 0 \leq |f| \leq wW - f_x \\ \sqrt{\frac{1}{2} \left[ 1 - \sin \frac{\pi(|f|-W)}{2f_x} \right]} & W - f_x \leq |f| \leq W + f_x \\ 0 & |f| \geq W + f_x \end{cases}$$

- The impulse response is

$$g(t) = 4\alpha \frac{\cos[(1+\alpha)\pi t/T] + \sin[(1-\alpha)\pi t/T] (4\alpha t/T)^{-1}}{\pi\sqrt{T} [1 - 16\alpha^2 t^2/T^2]}$$

where  $\alpha = f_x/W$ .

# Square Root Raised Cosine Pulse



*Raised cosine and root raised cosine pulses with roll-off factor  $\alpha = 0.5$ . The pulses are truncated to length  $6T$  and time shifted by  $3T$  to yield causal pulses.*

# $M$ -ary QAM

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- Quadrature Amplitude Modulation (QAM), the transmitted waveform in each baud interval takes on one of the following  $M$  waveforms

$$s_m(t) = \sqrt{\frac{2E_0}{T}}g(t) \left( a_m^c \cos(2\pi f_c t) - a_m^s \sin(2\pi f_c t) \right)$$

where

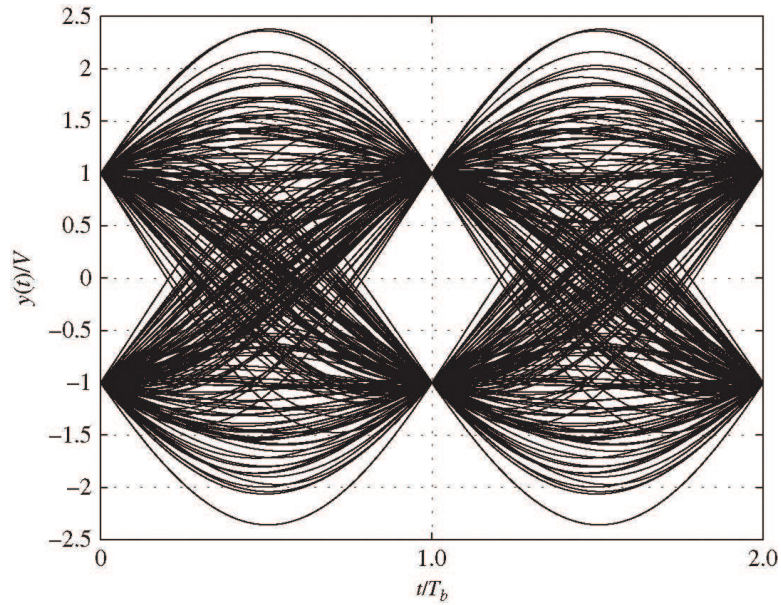
$$a_m^{\{c,s\}} \in \{\pm 1, \pm 3, \pm 5, \pm(M-1)\}$$

and  $2E_0$  is the energy of the signal with the lowest amplitude, i.e., when  $a_m^c, a_m^s = \pm 1$ .

- You have seen this before for the case  $g(t) = u_T(t)$ ; however, practical systems will use the root-raised cosine pulse for  $g(t)$ . Note that we use the normalization,

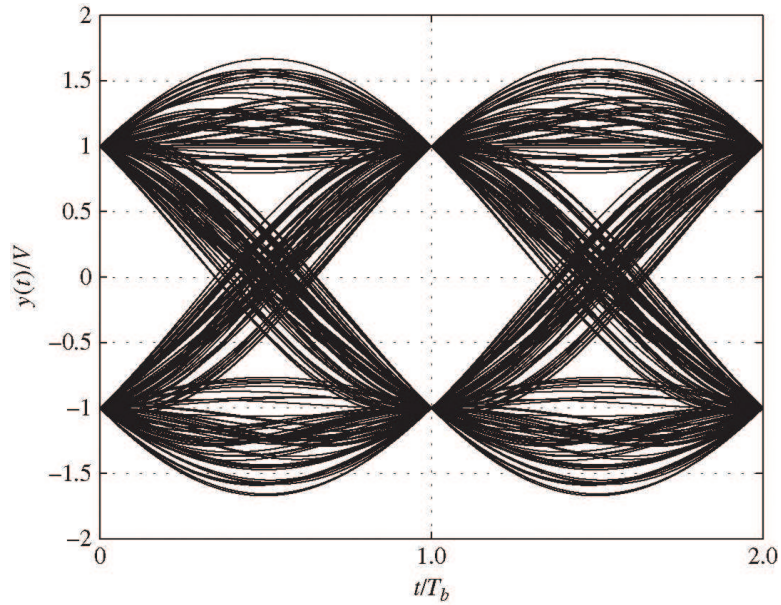
$$E_g = \int_{-\infty}^{\infty} g^2(t) dt = 1 .$$

# Eye Diagram with Ideal Nyquist Pulse



*Eye diagram when  $P(f)$  is an ideal low pass filter.*

# Eye Diagram with Raised Cosine Pulse



*Eye diagram when  $P(f)$  is a raised cosine filter.*